

# Microwave Electronics

## as an enabling information technology

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UNIVERSITÀ  
DEGLI STUDI  
FIRENZE

**DINFO**  
DIPARTIMENTO DI  
INGEGNERIA  
DELL'INFORMAZIONE



- Dal 23.12. 2011 svolgo l'attività di **Professore Associato di Elettronica (INGINF-01)** presso il DINFO, conferma in ruolo con decorrenza 23.12.2014;
  - Ambito di ricerca: **elettronica delle microonde e onde millimetriche**;
  - Didattica:
    - **Elettronica dei Sistemi a Radiofrequenza** CdS - Ingegneria Elettronica e TLC
    - **Dispositivo per la Micro e Nano Elettronica** CLM – Elettronica
  - Membro del collegio dei docenti del Dottorato di Ricerca *Pegaso* '**Smart Industry**'
- Ho ottenuto l'**Abilitazione Scientifica Nazionale di I Fascia**, per il settore concorsuale **09/E3 – ELETTRONICA** il **20 Luglio 2017**



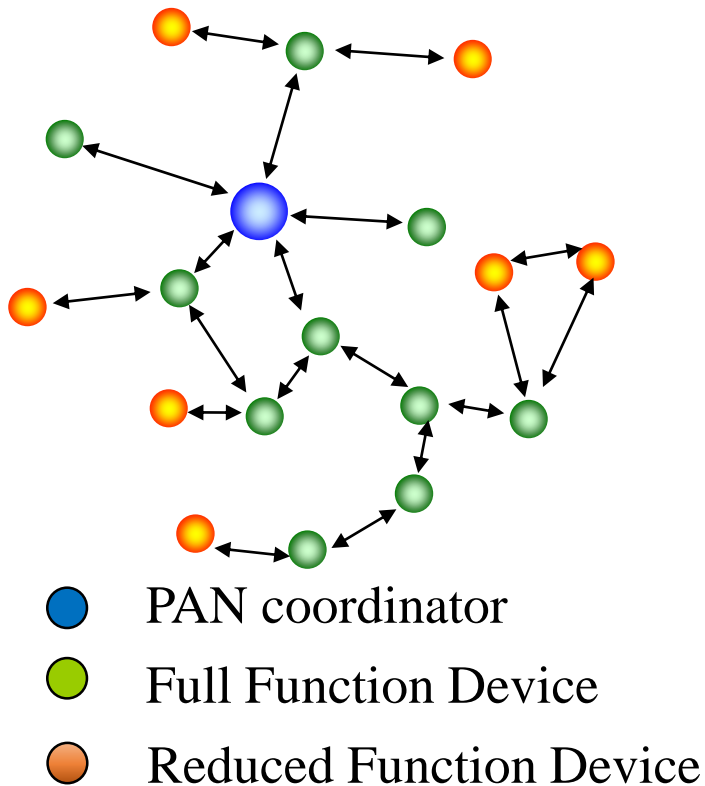
- Membro eletto della **Commissione di Indirizzo e Autovalutazione** del DINFO;
- Dal 13 Giugno 2017 ho assunto il ruolo di **Direttore del Centro Interdipartimentale per le Tecnologie e Microsistemi per la Sicurezza e Qualità Ambientale** dell'Università di Firenze;
- Dal 7 Giugno 2019 assume il ruolo di **Responsabile scientifico del Laboratorio Congiunto in “Tecnologie e Sistemi per l'Info-Mobilità”** tra la **Società Autostrade Tech** e **DINFO**;
- Membro del comitato di gestione del Centro di Ricerche interuniversitario **Microwave Engineering for Space Applications (MECSA)**

- Consocia **4 Dipartimenti UniFI** e **18 docenti/ricercatori/tecnici**
- Si occupa prevalentemente di attività di ricerca e disseminazione nell'ambito del **monitoraggio ambientale** per finalità di controllo e sicurezza



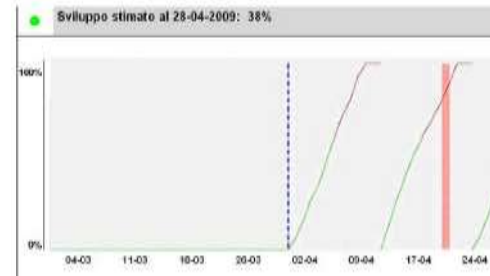
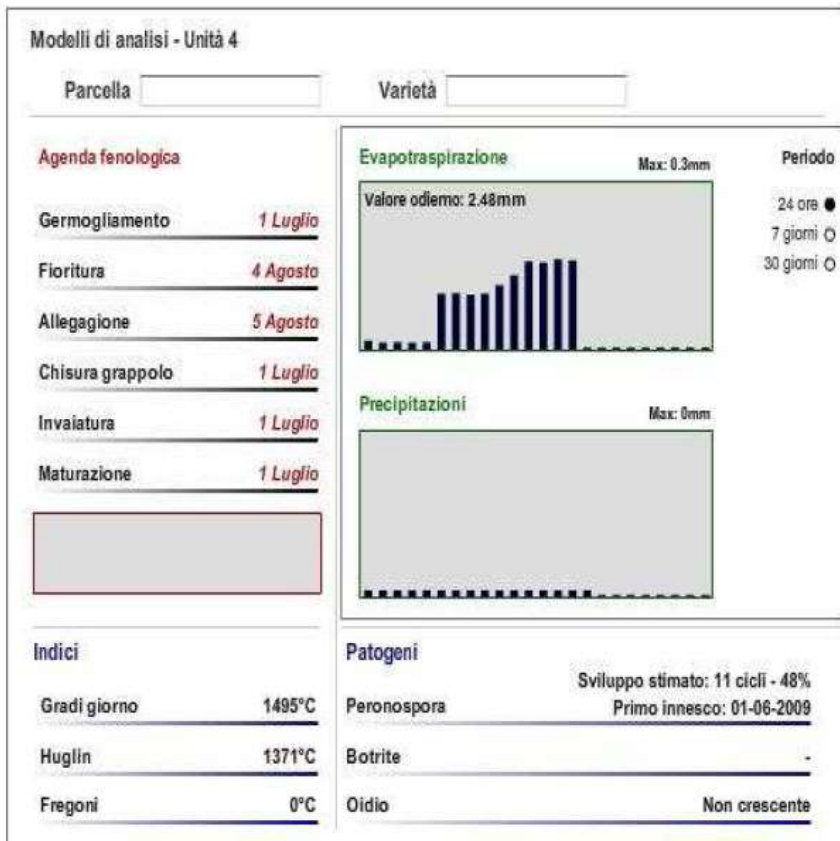
Impiego di wireless sensors network per il monitoraggio della vigna dell'azienda universitaria di Montepaldi

# Villa MONTEPALDI



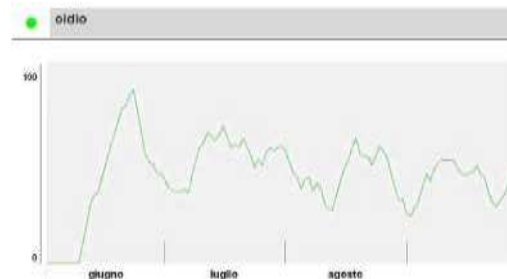
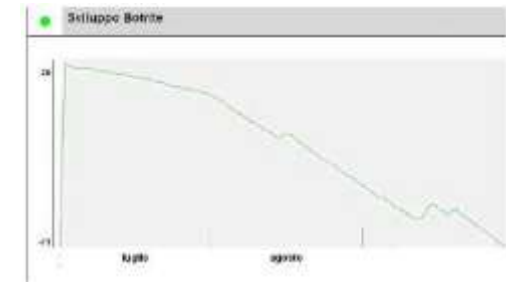


### Previsione degli attacchi di patogeni per la somministrazione adattiva di trattamenti



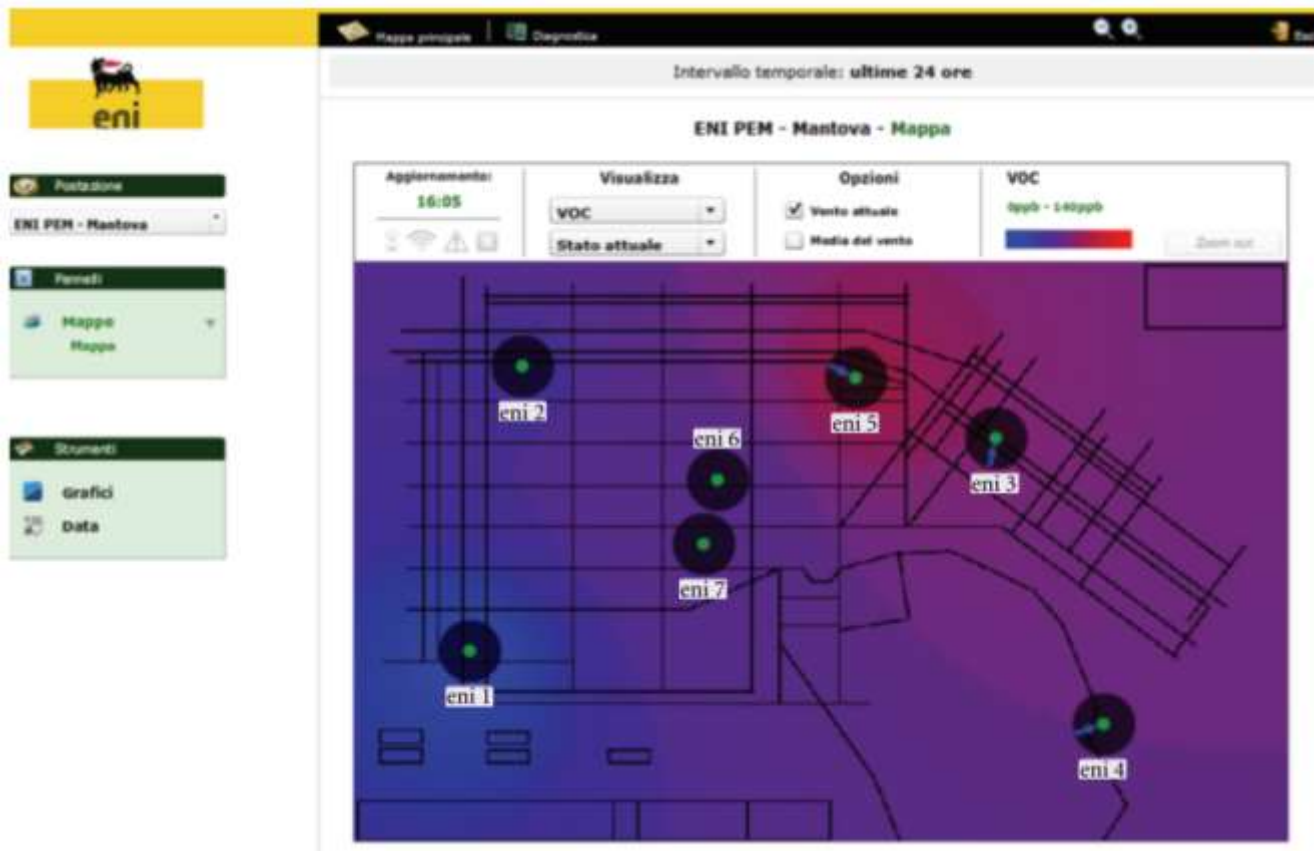
Previsione attacco Peronospera

Previsione attacco Botrite



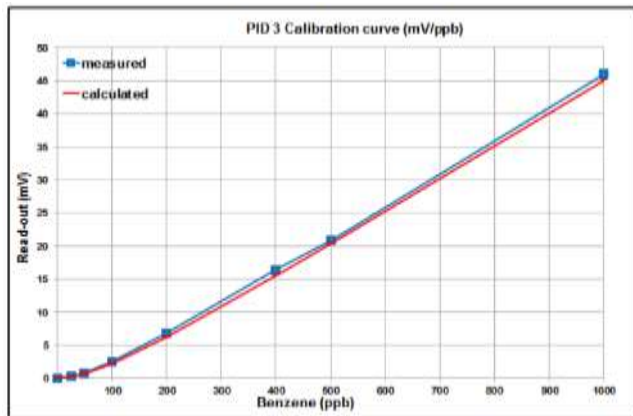
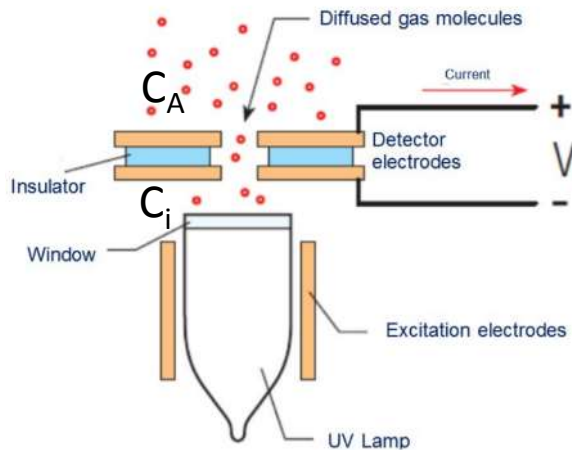
Previsione attacco Oidio

Distributed Integrated System for Volatile Organic Compound (VOC) Monitoring": rete presso lo stabilimento petrolchimico di Mantova



Photoionization detectors (PIDs) measure VOCs and other toxic gases in low concentrations from ppb up to 10,000 ppm.

Gas molecule ionization yields a current determined by opposite-polarity ions collected by a pair of electrodes.



- The PID operation principle is governed by the Fick's first law, which provide the analyte,  $J$ , diffusion

$$J = \frac{1}{A_C} \frac{\partial n(t)}{\partial t} = -D \frac{\partial C}{\partial x}$$

- Introducing the diffusivity length,  $L_d$ , and ionization time  $\tau_i$ :

$$J_D = \frac{1}{A_C} \frac{\partial n}{\partial t} \Big|_{x=0} = D \frac{(C_A - C_{i0})}{L_d}, \quad \frac{\partial C_i(t)}{\partial t} = K I_n \frac{\sigma}{S} C_i = K \frac{C_i}{\tau_i} = \frac{C_i}{\tau_i}$$

- The calibration process involves the readout measurements at various  $C_i$  (ppb)

$$\alpha_n = (C_i)_n = \frac{V_n}{S_{Vn}} = \frac{V_{OUTn}}{S_{Vn} \cdot G}$$

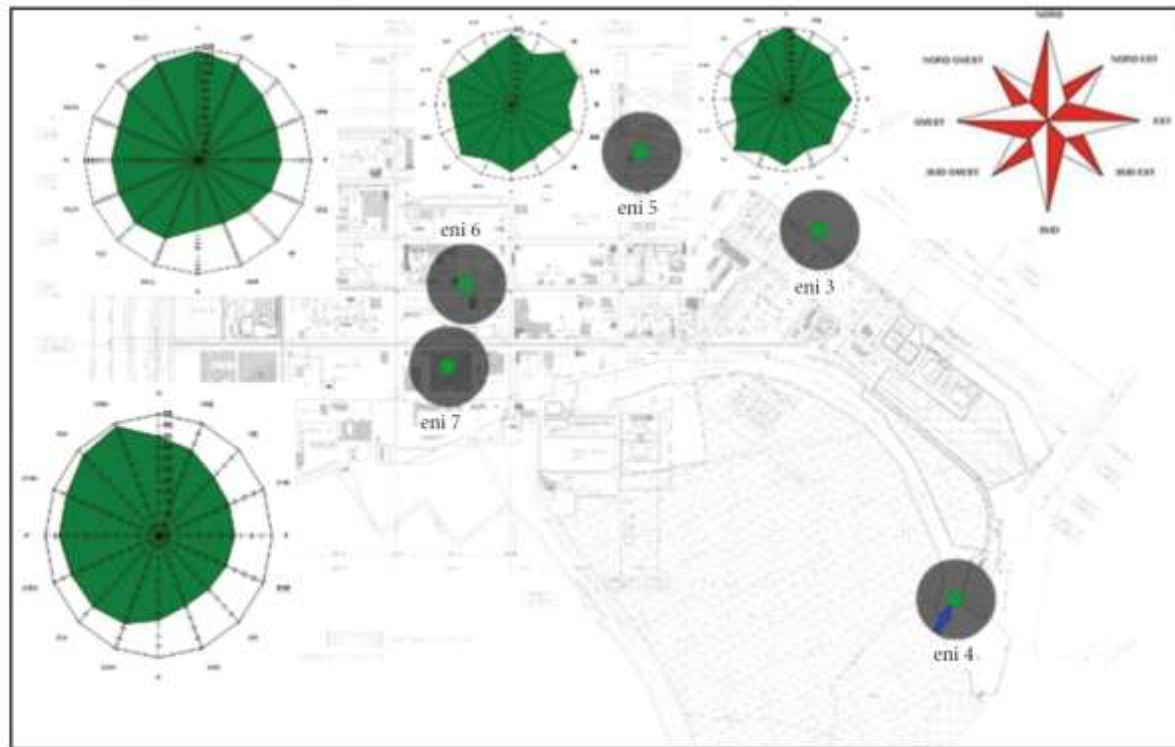
- then the classical PID zero/span calibration curve should be modified to represent the nonlinear behavior in the **low-ppb range**

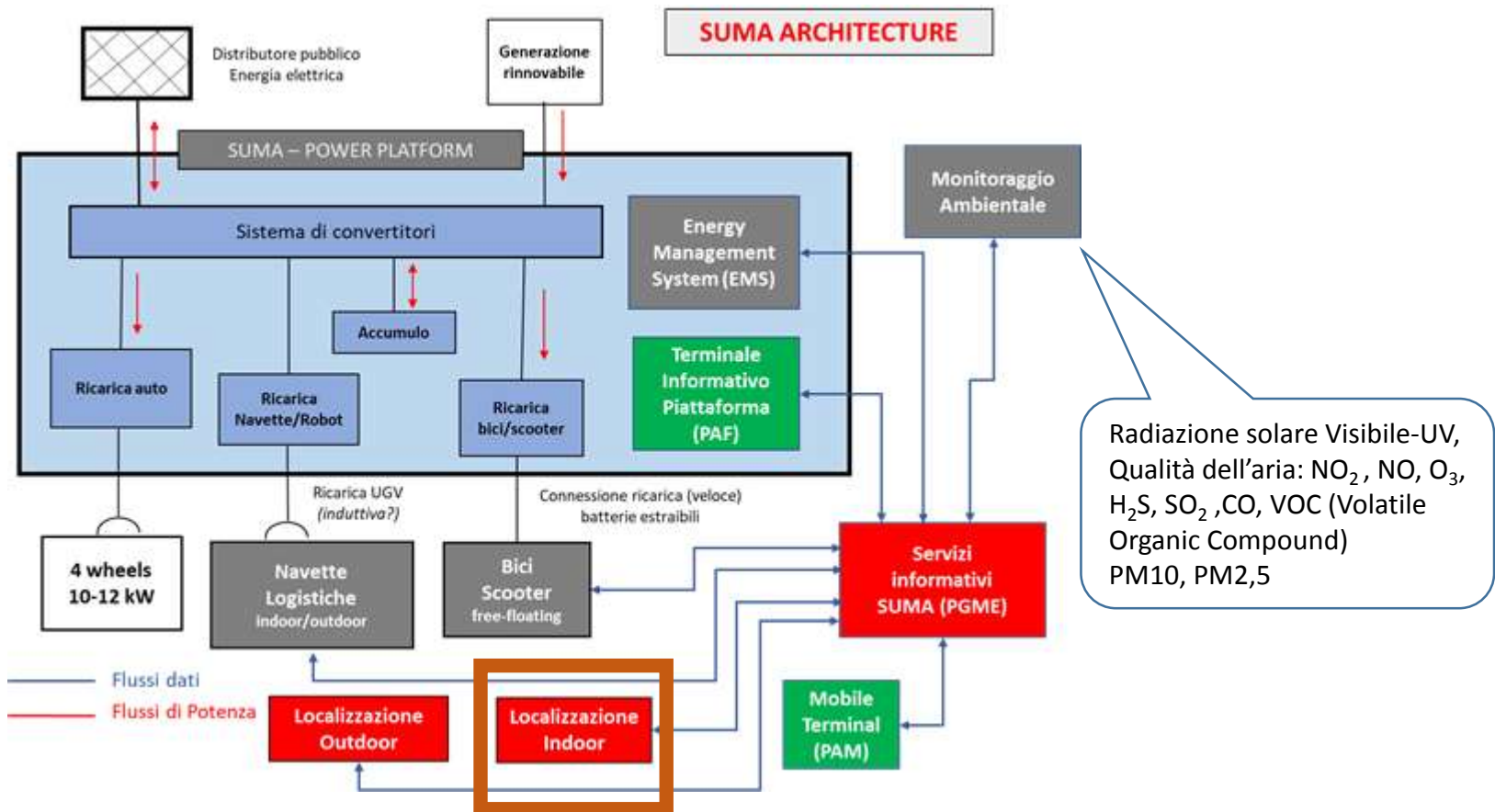
$$V(C_A) = \alpha S_V C_A = \frac{C_A^2}{C_A + C_o} S_V$$



“Distributed Integrated System for Volatile Organic Compound (VOC) Monitoring”: rete presso lo stabilimento petrolchimico di Mantova

Fusione dati VOC – dati ambientali (direzione e intensità del vento)





# Indoor wireless localization technology

- o Assuming a multi-beam radio device, (the anchor), an **anchors constellation reads an array of Received Signal Strength Indicator (RSSI)**,  $\dim(\text{RSSI})=N \times M$
- o the simplest analytical search Localization reduces to the solution of the following **Least Square Estimator**

The observation model is

$$RSSI_n = G_n(\hat{\theta}) + P_{inc} + w$$

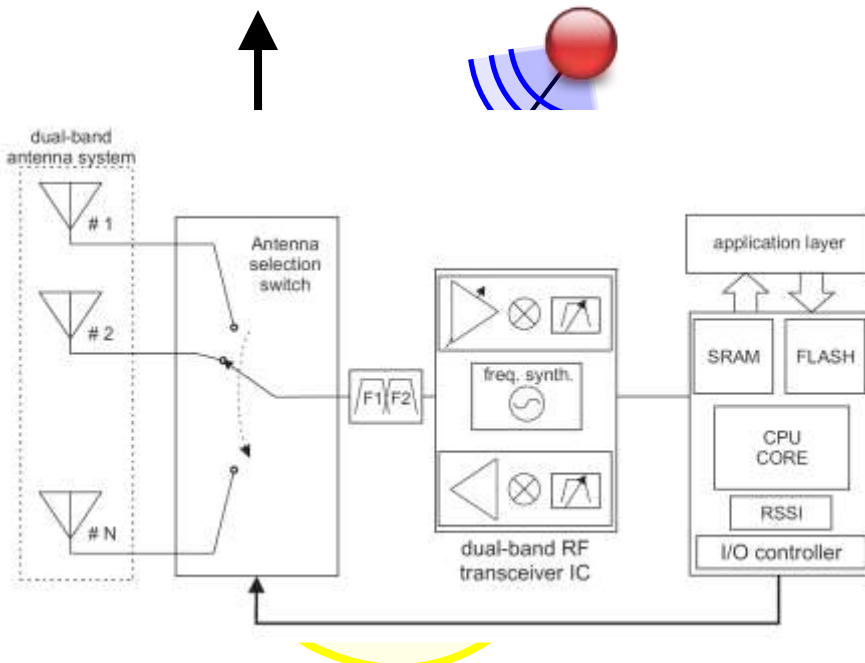
$s$  compared with the incident power from the anchor source in position  $(x, y)$ , at distance  $D$  from anchor

$$P_{inc}(D) = P_{tx}(x, y) + 20 \log(4\pi D / \lambda_0)$$

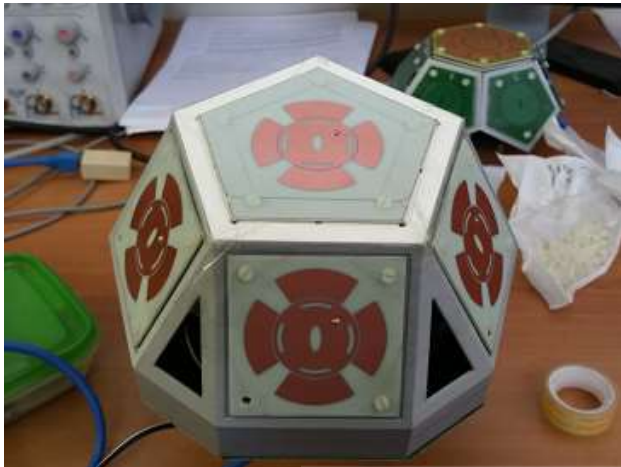
we assume the cost function the variance of difference between the steering vector and the observed signal map

$$C(x, y) = \frac{1}{MN} \sum_{i=1}^{MN} \left[ (s_i - m_i) - \frac{1}{MN} \sum_{j=1}^{MN} (s_j - m_j) \right]^2$$

$$(\hat{x}, \hat{y}) = \text{argmin} \{ C(x, y) \}$$



- By the Fisher Information Matrix (F) the accuracy of a DoA estimation is achieved *a-priori*
  - For the 2D case in exam the FIM is defined as

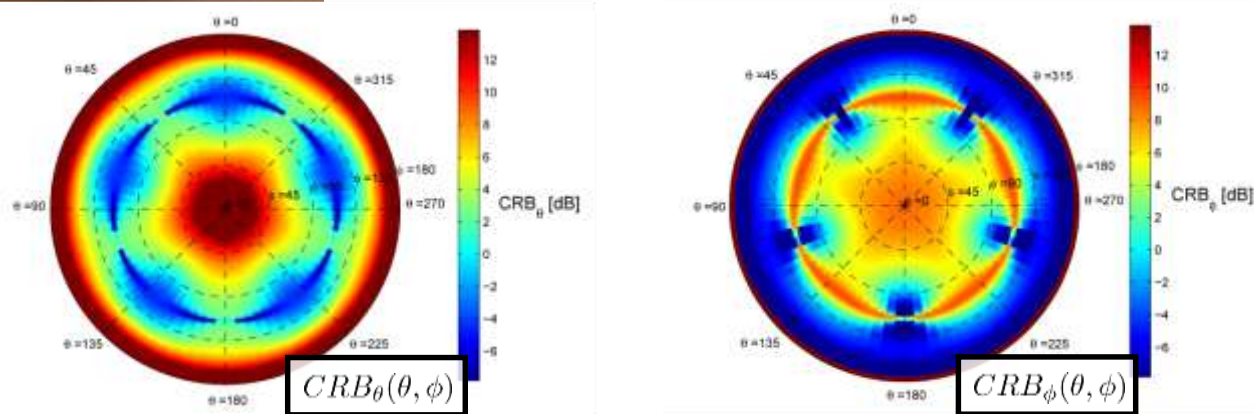


$$CRB_x(x, y) = [\mathcal{F}]^{-1}|_{2,2} = \sigma_{RSSI}^2 \frac{\sum_n^{NM} \left[ \frac{\partial G_n}{\partial x} \right]^2}{Det[\mathcal{F}]}$$

$$CRB_y(x, y) = [\mathcal{F}]^{-1}|_{1,1} = \sigma_{RSSI}^2 \frac{\sum_n^{NM} \left[ \frac{\partial G_n}{\partial y} \right]^2}{Det[\mathcal{F}]}$$

therefore, for any unbiased position estimator:

$$Var [E] \geq CRB(x, y) = CRB_x(x, y) + CRB_y(x, y)$$



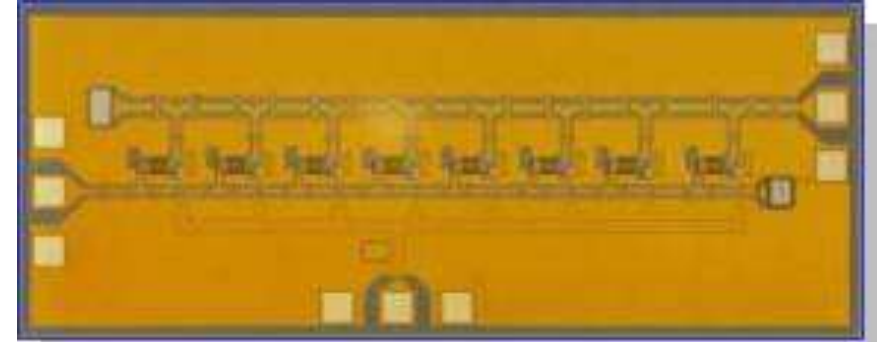


## A brief introduction

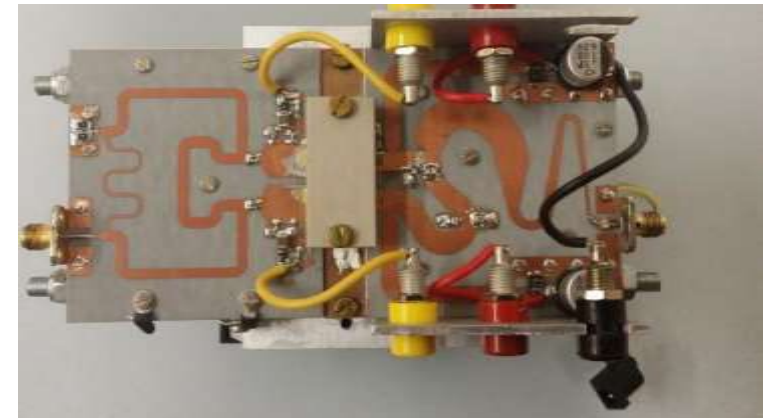
Example of systems and circuits investigated and developed



high dynamic range full-duplex DSRC transceivers



0.1 – 40 GHz bandwidth Travelling Wave  
Amplifier in 0.2 $\mu$ m GaAs HEMT technology



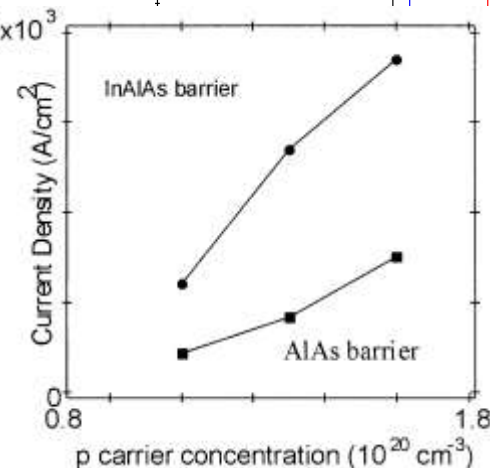
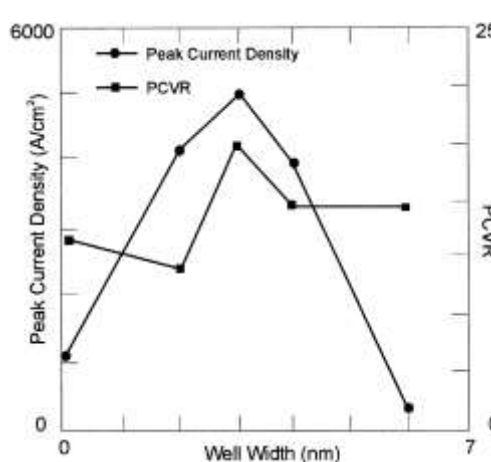
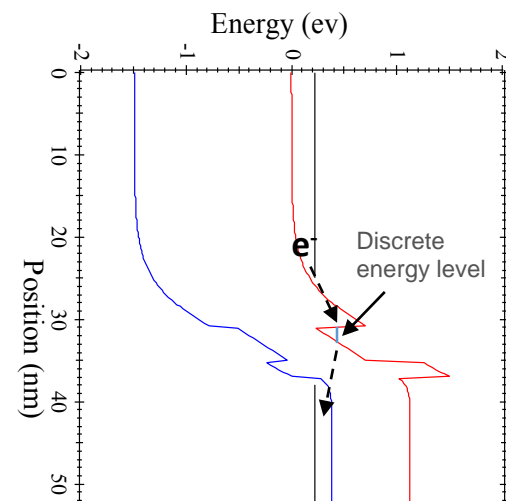
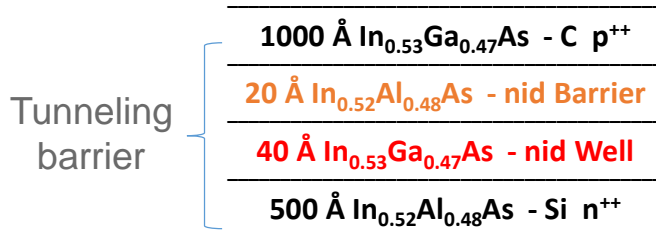
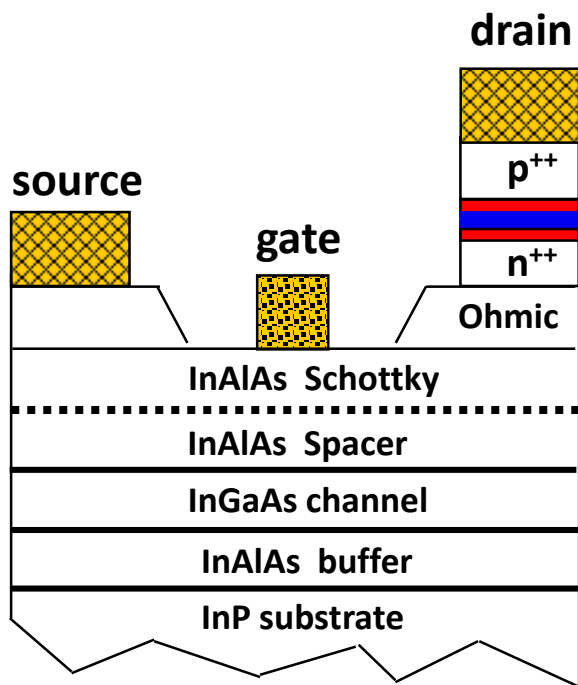
Doherty Power Amplifier DVBT 300 W peak power  
in Si-LDMOS technology



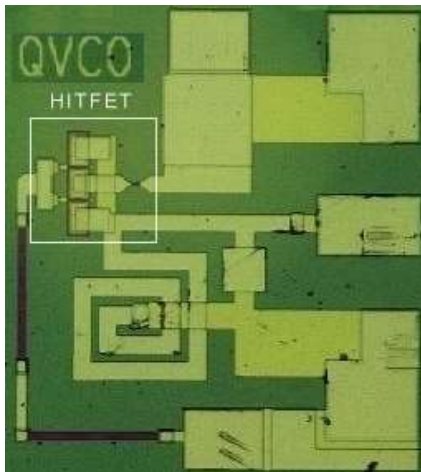


## A brief introduction

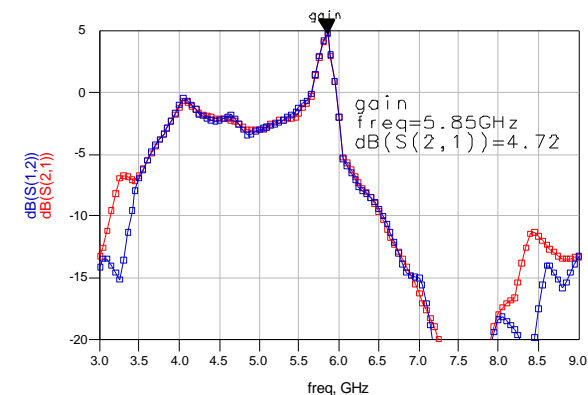
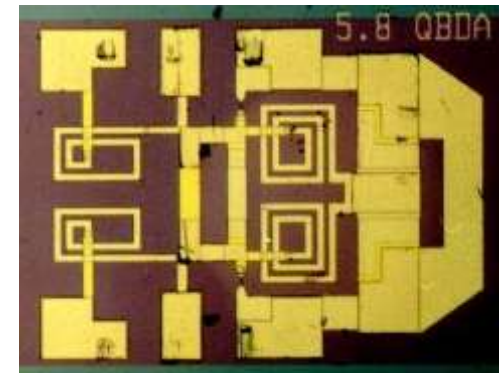
Device modeling investigation: quantum functional device based on *interband resonant tunneling*



The research was motivated by the potential development of building blocks in Microwave Monolithic Integrated Circuit (Quantum MMIC) technology operating at extremely low supply voltage and reduced number of devices



output frequency	6.18 GHz
output power	-16dBm
tuning range	140 MHz
SSCR	-105dBc/Hz @ 5MHz
efficiency	3%
power supply	850 $\mu$ W
supply voltage	500mV
die size	450x550 $\mu$ m <sup>2</sup>





**DINFO**

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# Nonlinear Dynamic Microwave Systems Characterization

at the “RF nonlinear characterization group” of the National Institute for  
Standard and Technology, Boulder (CO) USA



Prof K. C. Gupta, Ale, Dr. J. Jargon, and Dr K. Ramley

## A brief introduction

A general nonlinear system with memory is described by the multidimensional convolution integral, i.e. the Volterra Series

$$i(t) = \sum_{n=1}^N a_n \int_{-\infty}^{+\infty} \cdots \int_{-\infty}^{+\infty} h_n(\tau_1, \dots, \tau_n) v(t - \tau_1) \dots v(t - \tau_n) d\tau_n \dots d\tau_1$$

with  $N=1$  it describes a linear dynamic system.

*In the case of system memory duration  $\tau_\infty$  small compared to the inverse of excitation signal bandwidth  $B_W \rightarrow B_W \times \tau_\infty \ll 1$ , the series converges to the **Modified Volterra Series***

$$i(t) = F_{DC}(v(t)) + \int_0^{\tau_m} h(v(\tau), \tau) [v(t - \tau) - v(t)] d\tau$$



## A brief introduction

Under the assumption of the small-memory the term  $[v(t - \tau) - v(t)]$  becomes a linearization of the large-signal,  $v_{LS}(t)$ , applied to the system

$$i(t) = F_{DC}(v(t)) + \sum_1^N f^{(n)} \cdot \frac{d^n v}{dt^n}$$

with

$$f^{(n)}(v(t)) = \frac{1}{n!} \int_0^{\tau_m} h(v, \tau) \cdot \tau^n d\tau$$

coefficients to be determined.

The model can be conveniently identified in  
frequency domain

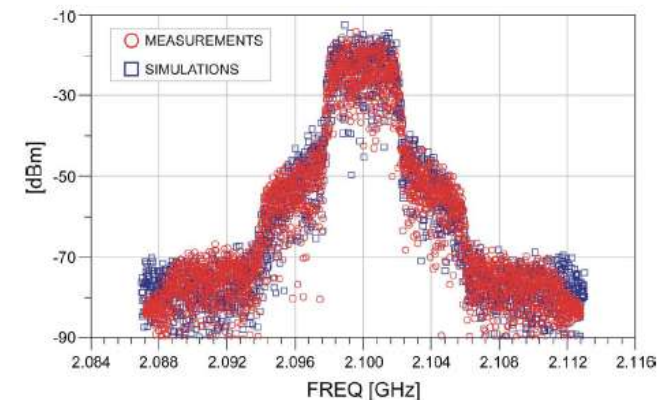
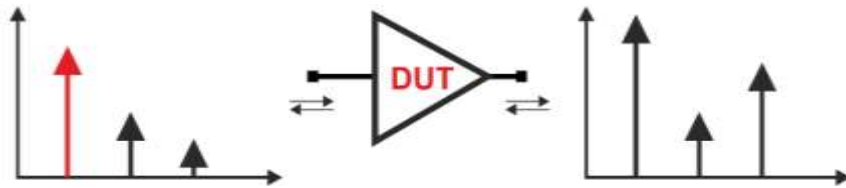


Fig. 20. Comparison between simulated and modeled single carrier WCDMA at 2.1 GHz.



## Transforming into the frequency domain and introducing the concept of waves,



$$b_{1,k} = F_{1,k} (a_{1,1}, a_{1,2}, \dots, a_{2,1}, a_{2,1}, \dots)$$

$$b_{2,k} = F_{2,k} (a_{1,1}, a_{1,2}, \dots, a_{2,1}, a_{2,1}, \dots)$$

the linearization about the Large-Signal Operating Point (LSOP), lead to

- $i$ : number of system port;  $k$ : index of the harmonic
- If only one incident pseudo-wave,  $a_{1,1}$ , is large then the other smaller inputs can be linearized about the large-signal response of  $F_{i,k}$  to only  $a_{1,1}$ . **includes exact nonlinear mapping**

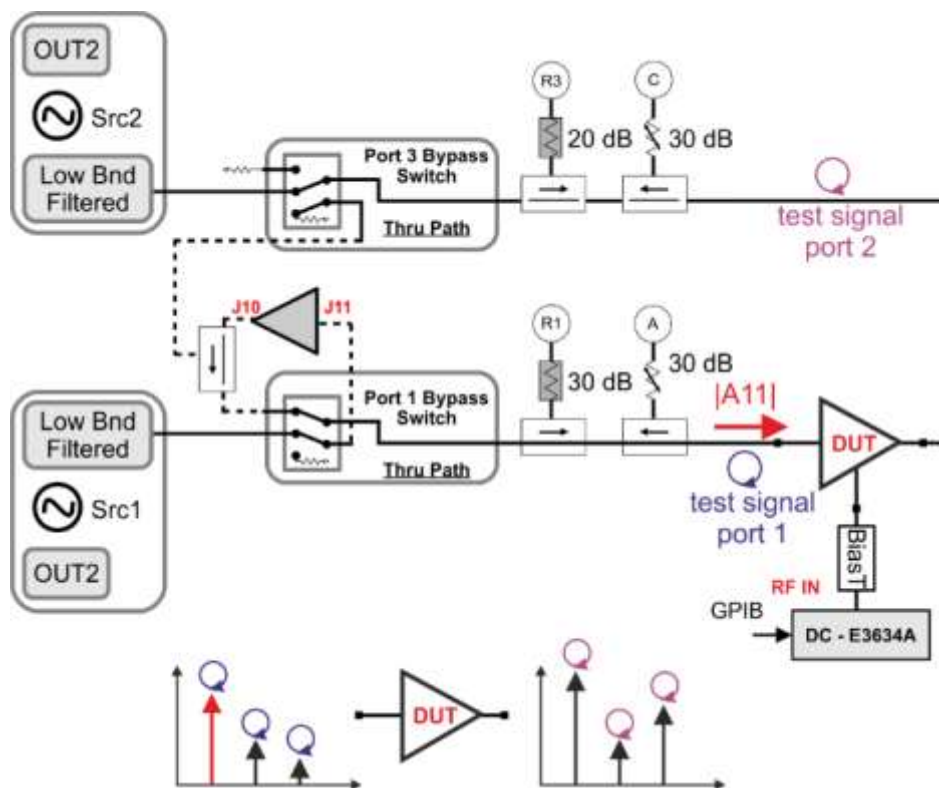
$$b_{i,k} = F_{i,k} (|a_{1,1}|, a_{1,2}P^{-2}, a_{1,3}P^{-3}, \dots) P^k \approx F_{i,k} (|a_{1,1}|, 0, 0, \dots) P^k$$

$$+ \sum_{k,l \neq (1,1)} \left[ \left. \frac{\partial F_{i,k}}{\partial (a_{kl}P^{-l})} \right|_{|a_{11}|} \cdot a_{kl}P^{k-l} + \left. \frac{\partial F_{i,k}}{\partial (a_{kl}P^{-l})^*} \right|_{|a_{11}|} \cdot a_{kl}^*P^{k+l} \right]$$

**to totally linear non-analytic map**

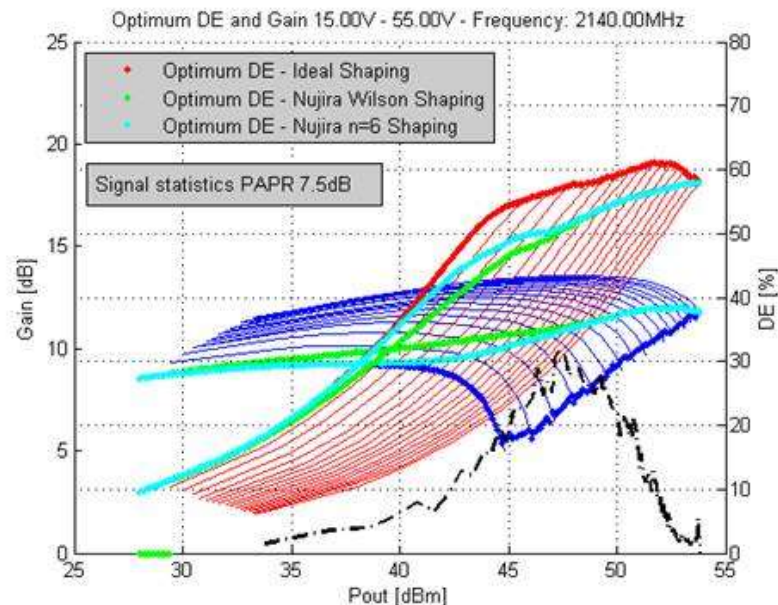
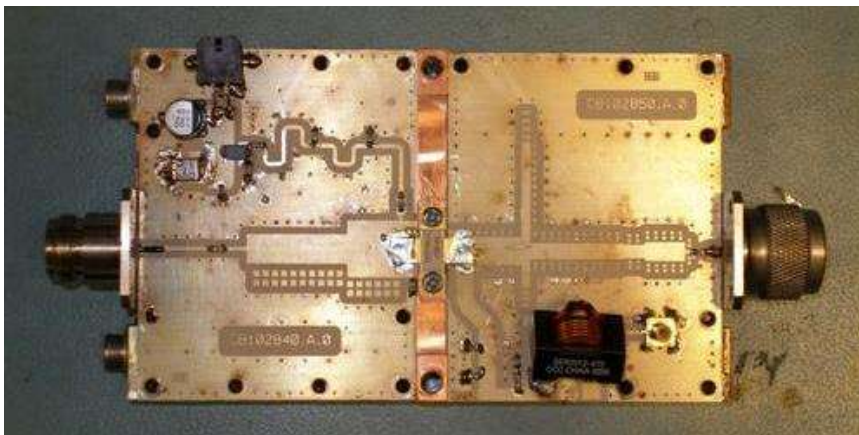
$$P = \frac{a_{1,1}}{|a_{1,1}|} = e^{j \cdot \arg(a_{1,1})}$$

- The setup is based on a calibrated multi-port transmitters - coherent receivers
- The absolute value of harmonics amplitude and phase is measured
- The technique: injects a drive large-signal at the device input and sequentially a test signal at each port and to all fundamentals and harmonics.
- The test signal phase is rotated at steps around 360 degrees



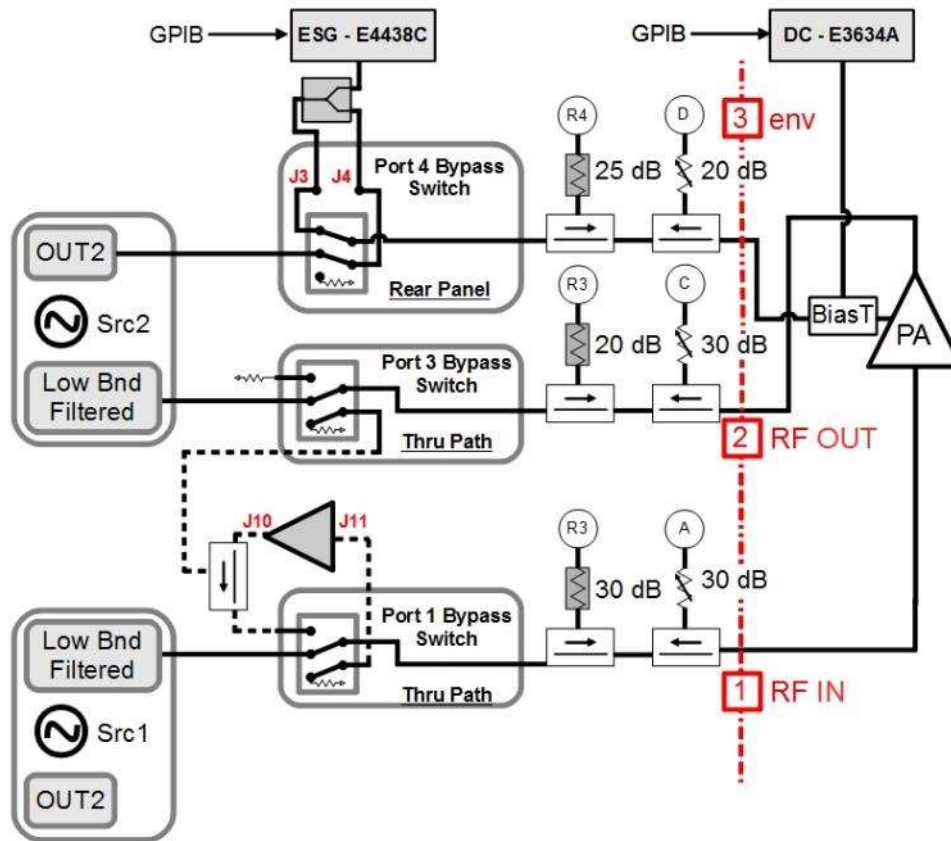
Dual-band GaN based ET-PA, developed by **probability conscious approach**

- ❑ The signal distribution imposes the estimation of the optimum impedance on mean value basis
- ❑ Shaping table, that is the law  $V_{dc}$  vs  $P_{in}$ , is critical in the ET-PA



## 3-port ET-PA dynamic model of

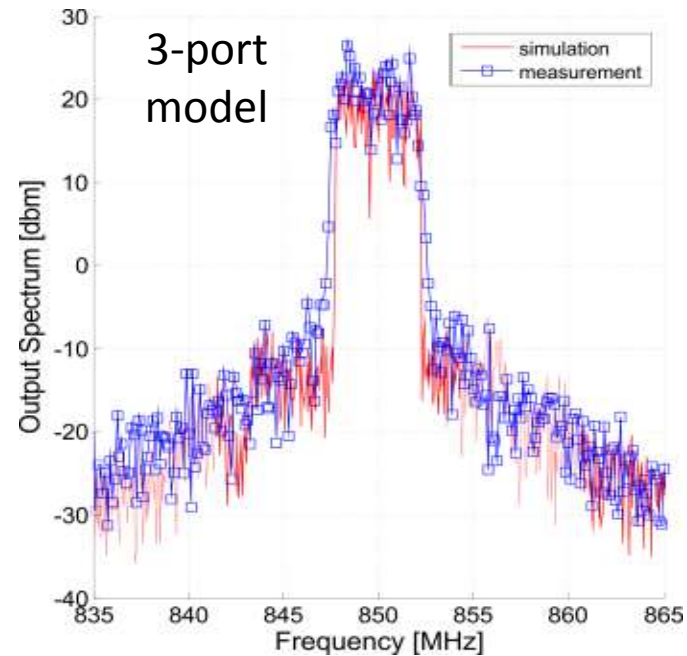
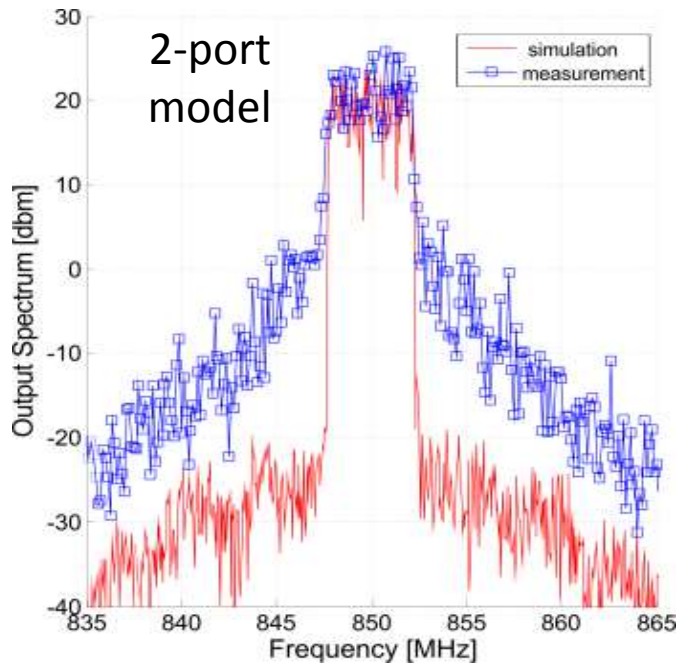
- Extracted by a 3-channel Nonlinear VNA based set up







# Nonlinear Vector Characterization: Envelope Tracking PA modeling

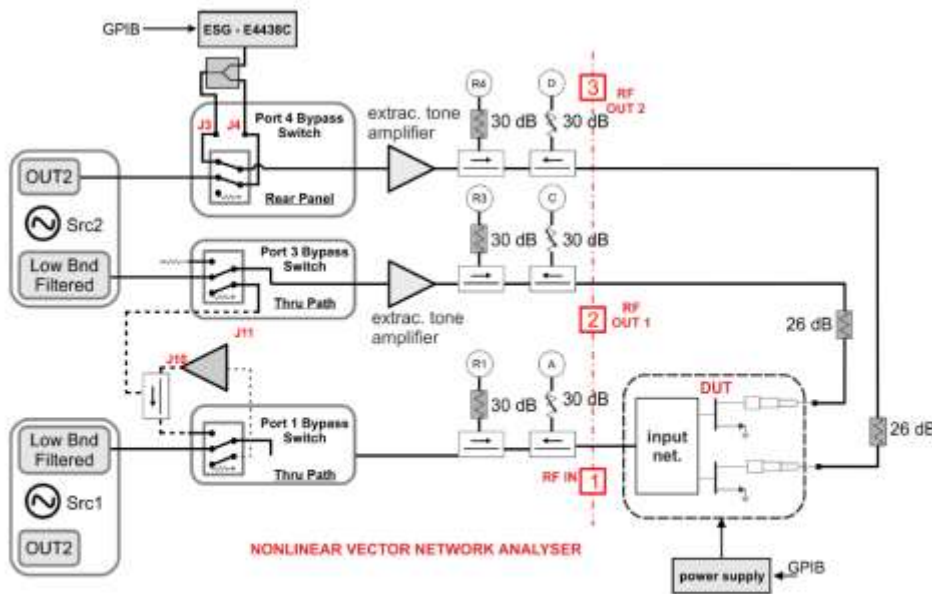


Comparison between measured and simulated LTE5 spectra at the ET system output for at 35.5 dBm output power.

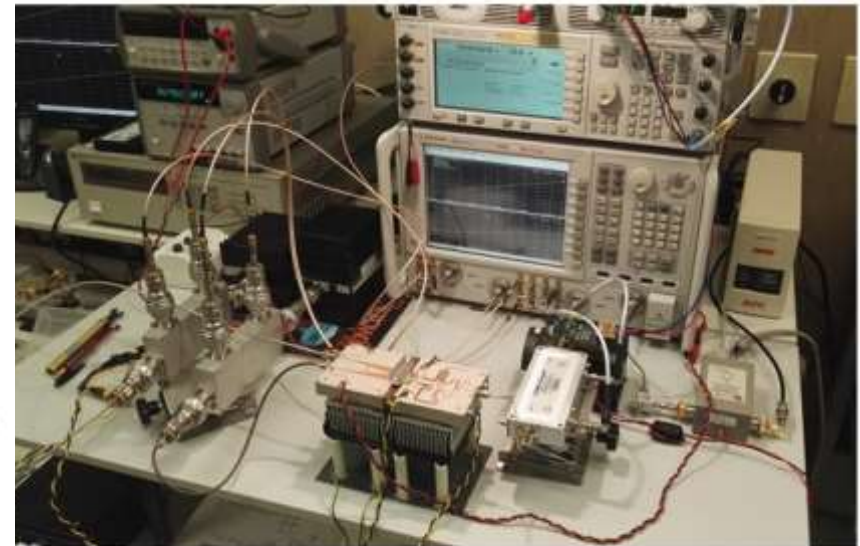
model	Measured [dB]		Simulated [dB]	
	ACLRlow	ACLRup	ACLRlow	ACLRup
<b>2-port</b>	-27.1	-25.3	-44.2	-44.2
<b>3-port</b>	-32.0	-29.1	-31.1	-31.1



## Si-LDMOS UHF Doherty High-Power Amplifier Design by 3-port subcircuit characterization

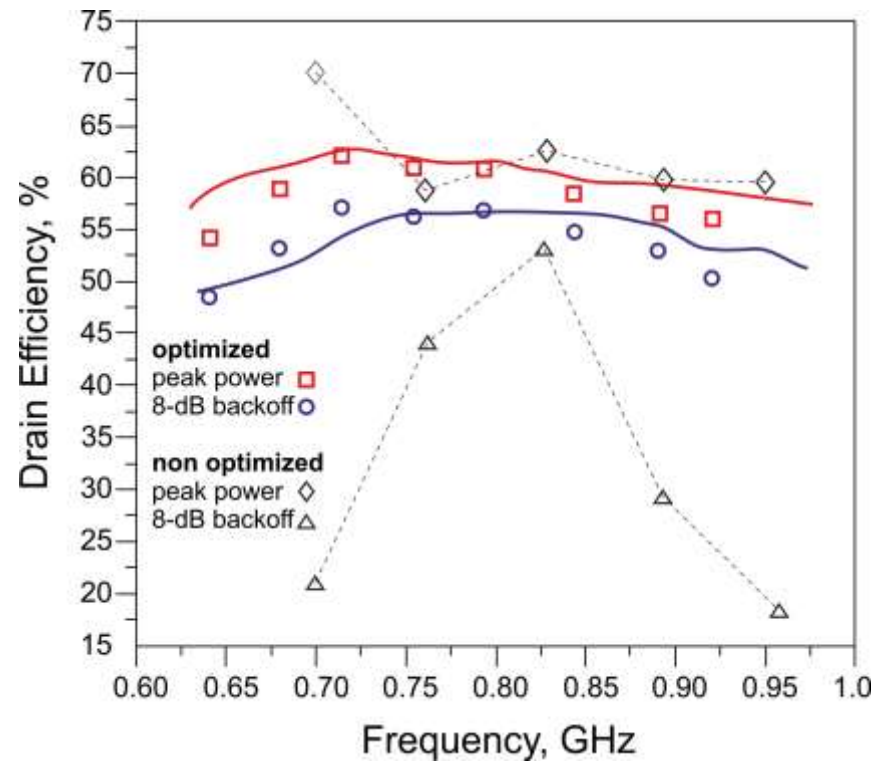
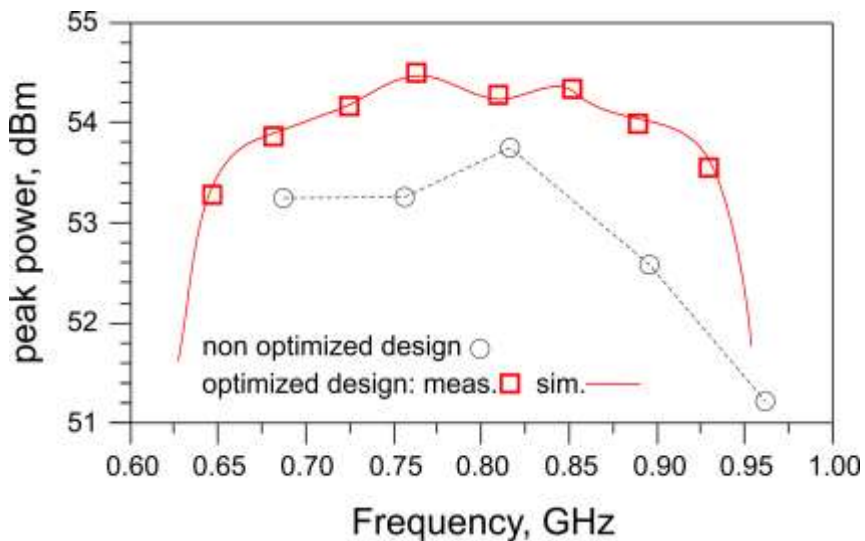


(a) Schematic of the 3-port NVNA based setup for the RF devices pair characterization.



(b) Picture of the 3-port NVNA set-up

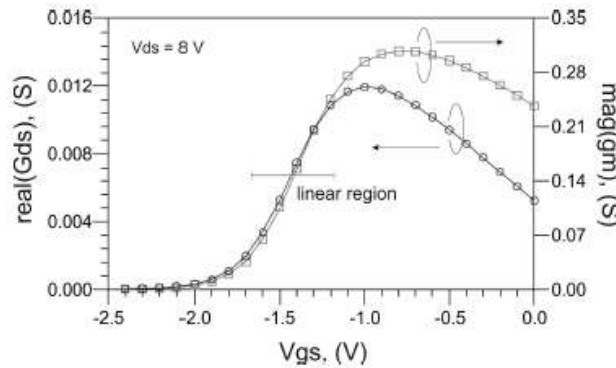
## Si-LDMOS UHF Doherty High-Power Amplifier Design by 3-port subcircuit characterization



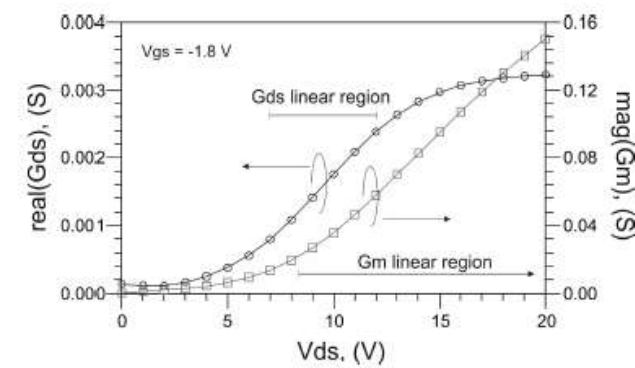
- Gallium Nitride (GaN) is an emerging s.c. technology for high power, high frequency applications
- We investigated its properties for highly linear Ka-band GaN-on-Si **MMIC Down-Conversion Active Balanced Mixer** for Radar Applications
- The conversion properties of a GaN-HEMT contains the LO

$$\begin{aligned}
 I_{ds} = & I_{ds}^{DC} + g_m v_{gs} + g_{ds} v_{ds} + \frac{1}{2} \frac{\partial g_m}{\partial v_{gs}} v_{gs}^2 + \frac{1}{2} \frac{\partial g_{ds}}{\partial v_{ds}} v_{ds}^2 \\
 & + \frac{\partial g_m}{\partial v_{ds}} v_{gs} v_{ds} + \frac{1}{6} \frac{\partial^2 g_m}{\partial^2 v_{gs}} v_{gs}^3 + \frac{1}{2} \frac{\partial^2 g_{ds}}{\partial^2 v_{gs}} v_{gs}^2 v_{ds} + \frac{1}{2} \frac{\partial^2 g_m}{\partial^2 v_{ds}} v_{gs} v_{ds}^2 + \frac{1}{6} \frac{\partial^2 g_{ds}}{\partial^2 v_{ds}} v_{ds}^3
 \end{aligned}$$

conversion     
 2<sup>nd</sup> order intermodulation     
 Taylor expansion, where the term  $v_{gs}$  contains the LO     
 Vds is set to 0 by a resonant short circuit



(a) Function of static drain voltage



(b) Function of static source voltage

Fig. 1. Simulation of the quasi-static  $g_m$  and  $g_{ds}$  device behavior.



- Gallium Nitride is an emerging semiconductor technology for high power, high frequency applications
- We have investigated its properties for highly linear Ka-band GaN-on-Si MMIC Down-Conversion Active Balanced Mixer for Radar Applications
- The conversion properties of a GaN-HEMT are described by the Taylor expansion, where the term  $v_{gs}$  contains the LO

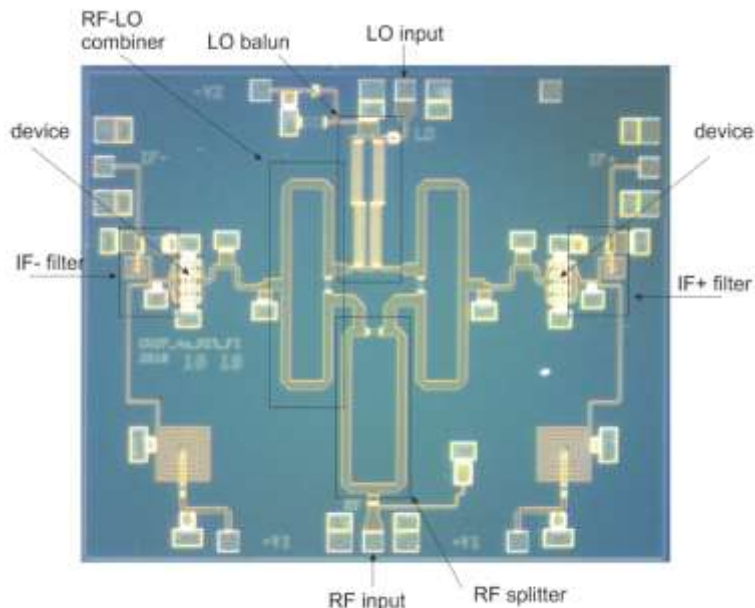


Fig. 3. The balanced mixer prototype chip photograph

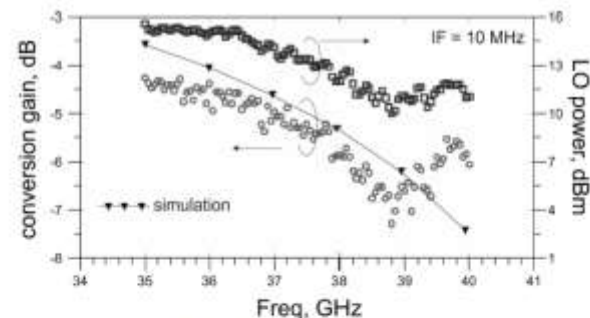
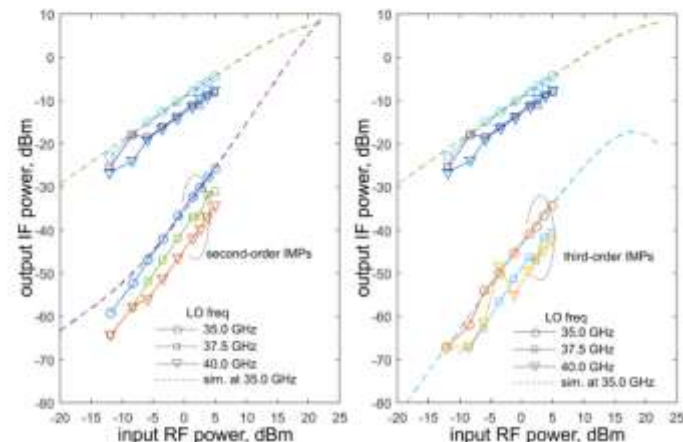


Fig. 4. Measured CG with calibrated 4-port VNA in mixer vector mode.



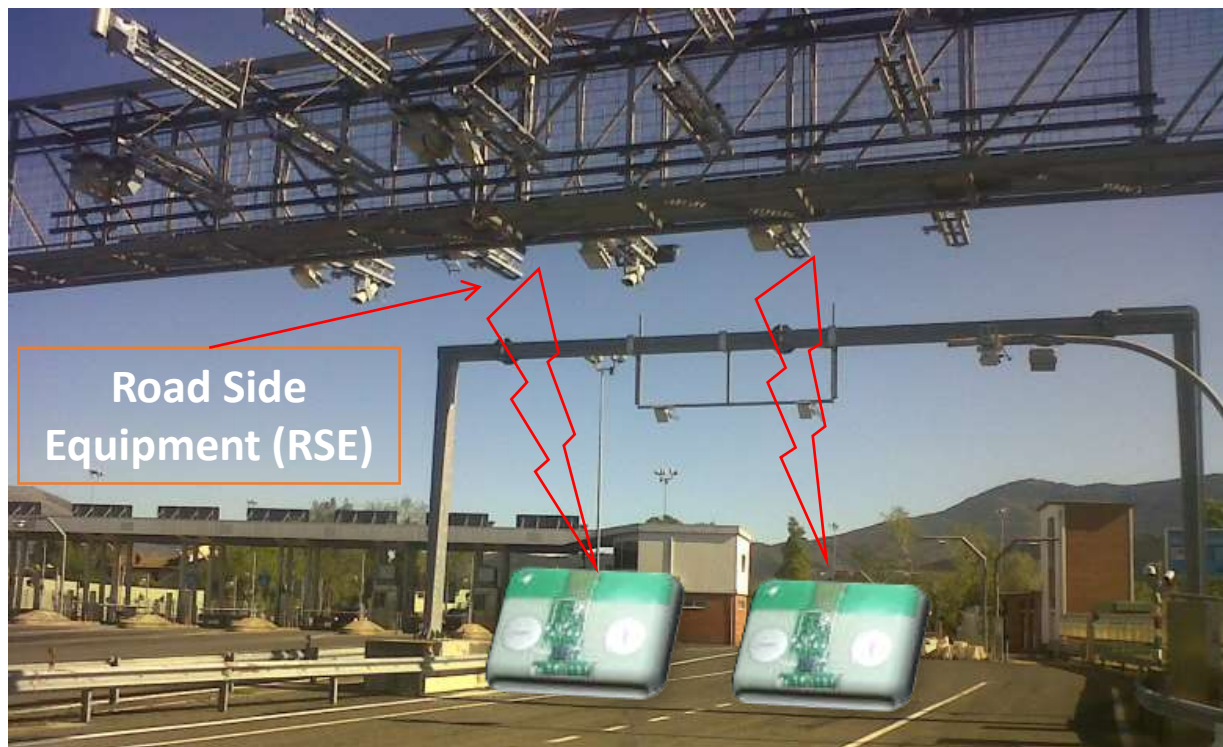
(a) IMP2 and down-conv. signals (b) IMP3 and down-conv. signals



## Sistema multi-lane free-flow per il pedaggio autostradale



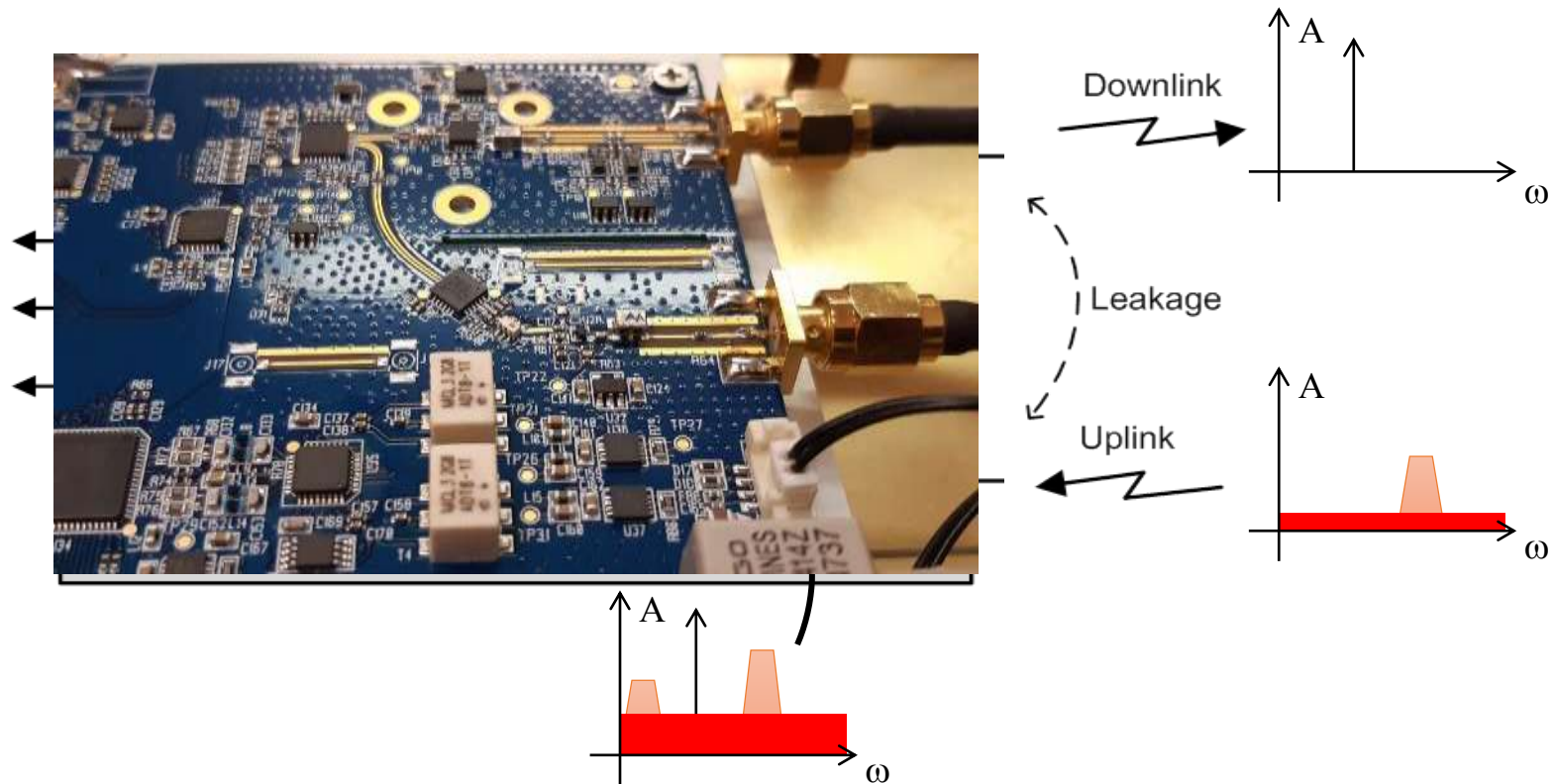
On-board unit)



Road Side  
Equipment (RSE)

Attività svolta nell'ambito del **Laboratorio Congiunto “Tecnologie e Sistemi per l'Info-Mobilità”** tra **DINFO** e la **Società Autostrade-Tech**

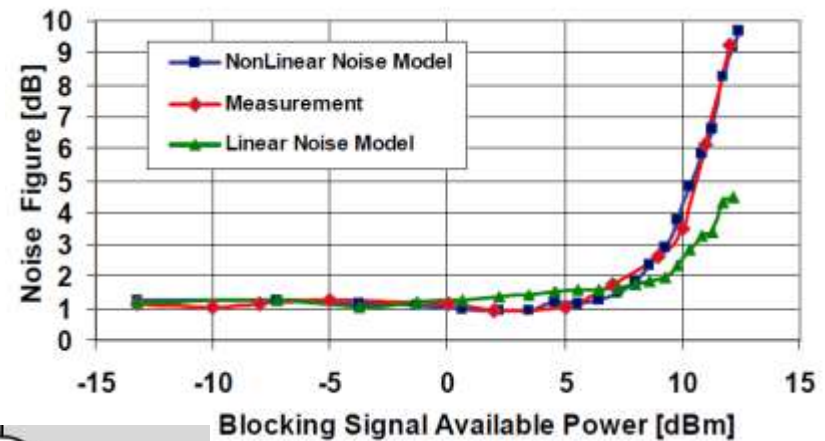
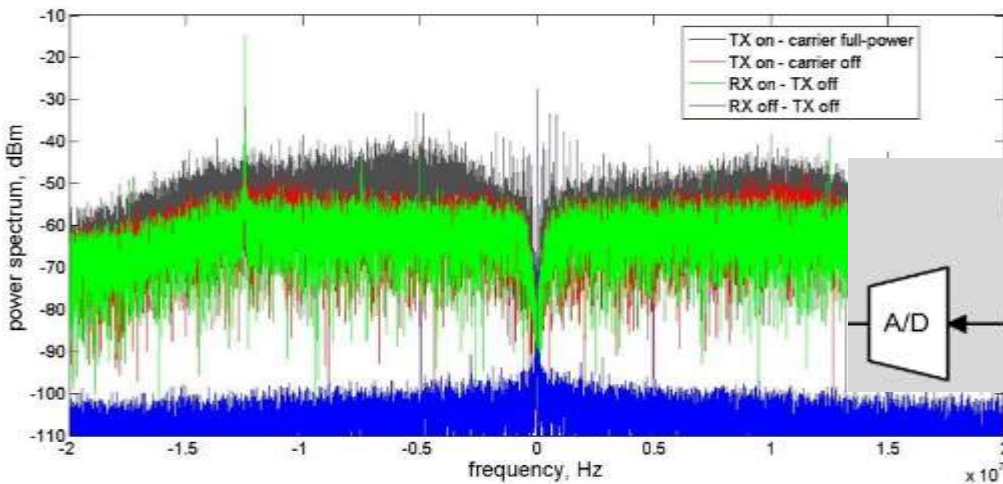
- The self-interference determines
  - an increase of LNA noise figure
  - higher levels of the required down converter SFDR



## NF increases with the interference strength

- Example of GaAs PHEMT LNA driven beyond P-1dB
  - Linear model: bias dependent noise source modulation
  - Nonlinear model: noise source correlation and conversion

DSRC spectrum at the Rx baseband: subcarrier at 1.5 MHz  
signal 16 ks digitized by a 16 bit ADC at 40 Msps



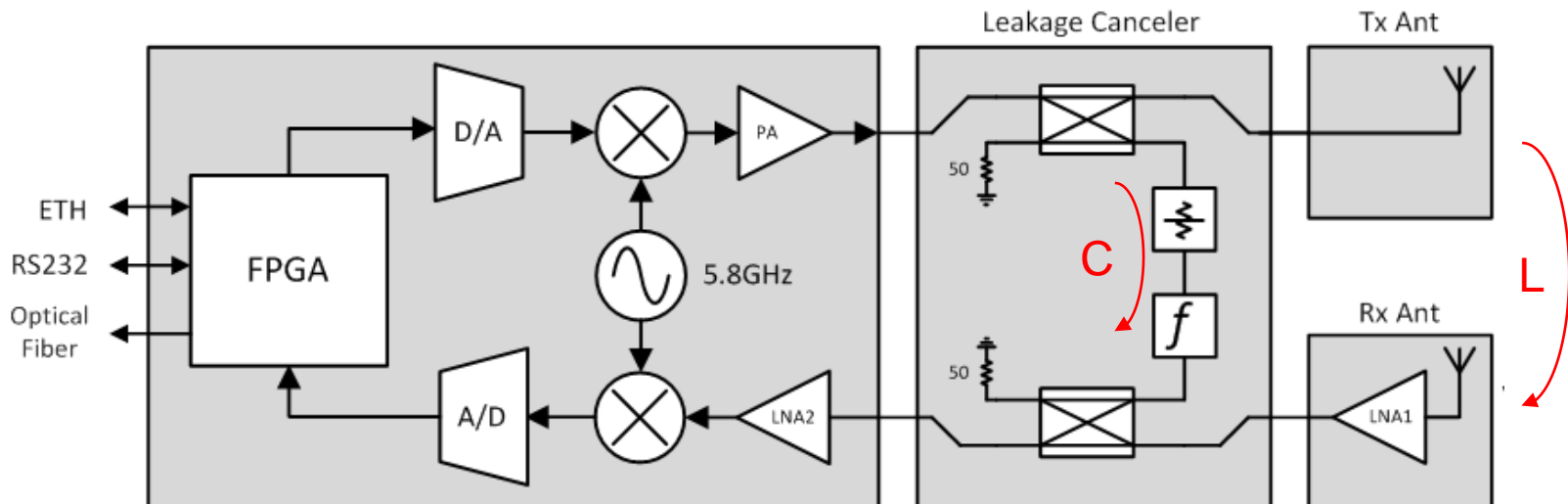
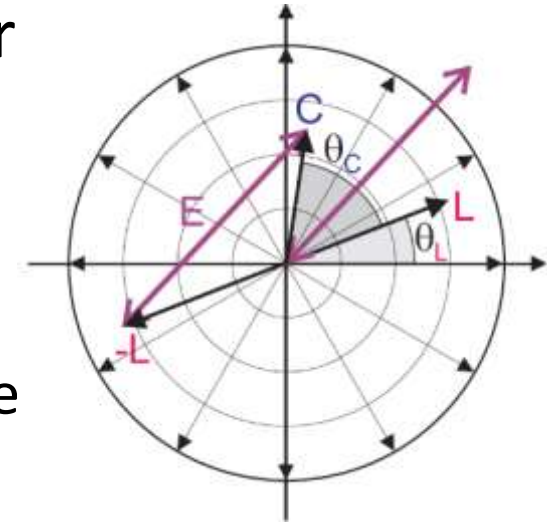
$$F = \frac{N_0^{(Nlin)}}{K_B T G_T^{(Nlin)}}$$



- Canceler operation principle: from the Car theorem

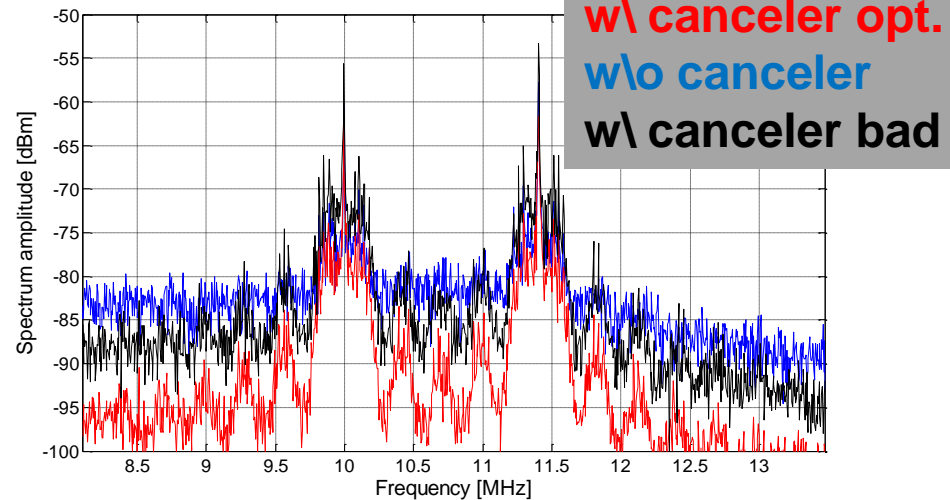
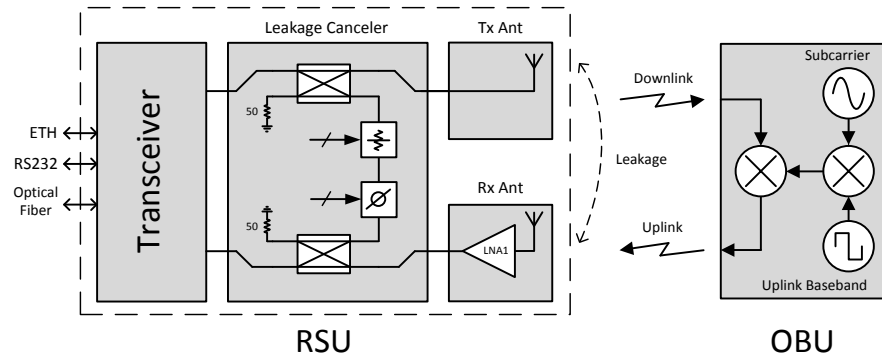
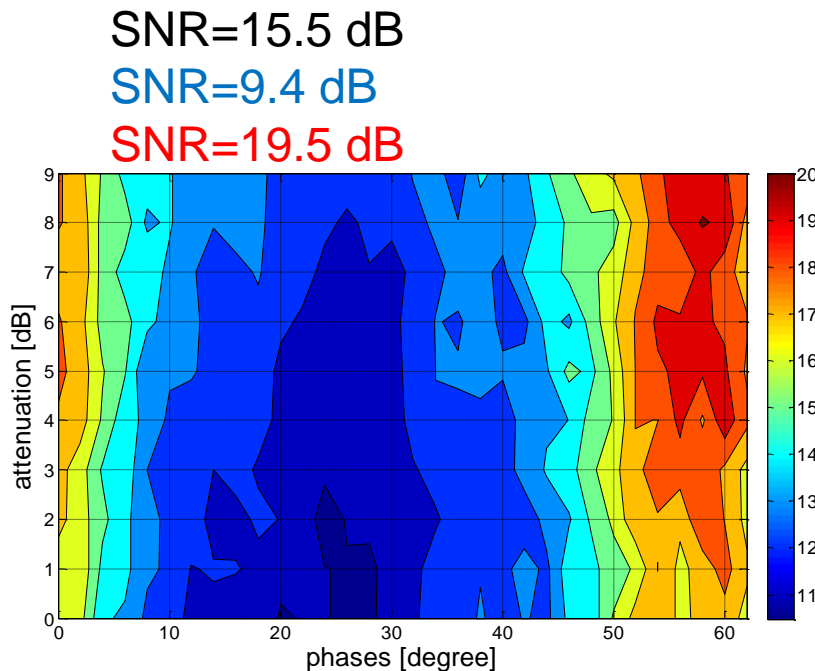
$$E = \sqrt{|L|^2 + |C|^2 + 2|L||C| \cos(\theta_C - \theta_L)}$$

- For  $L/C=1$  and  $\theta_C - \theta_L = \pi$  the cancellation of the perfect



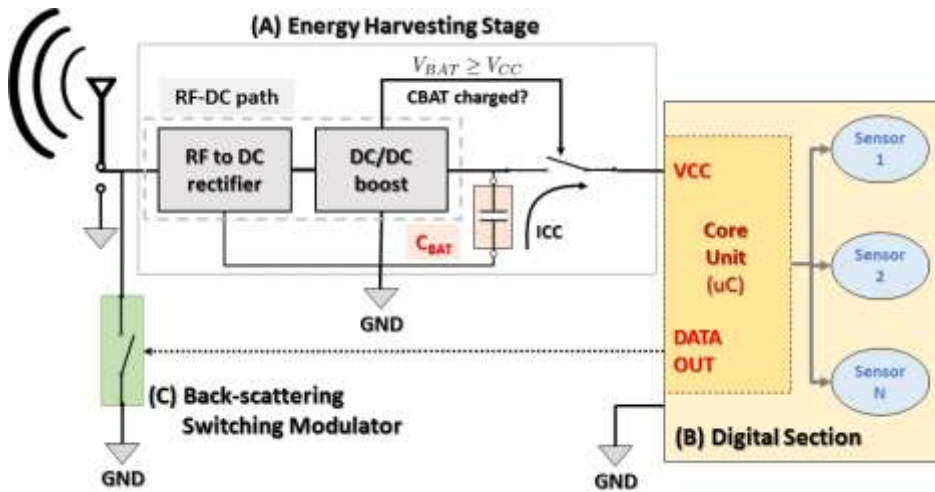


- The canceler for DSRC in real case can effectively reduce the interference

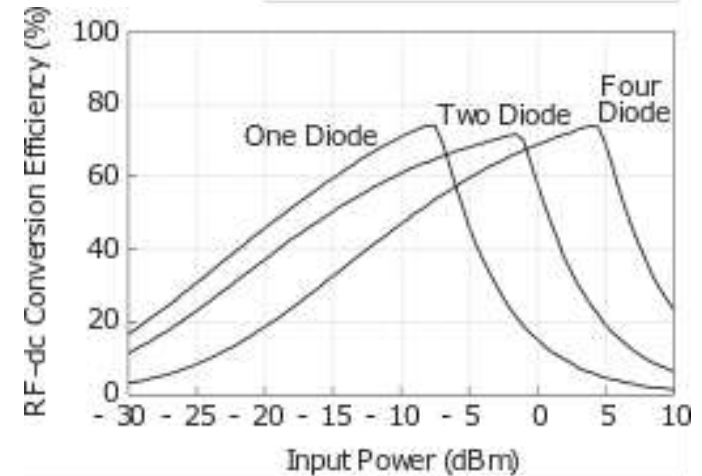
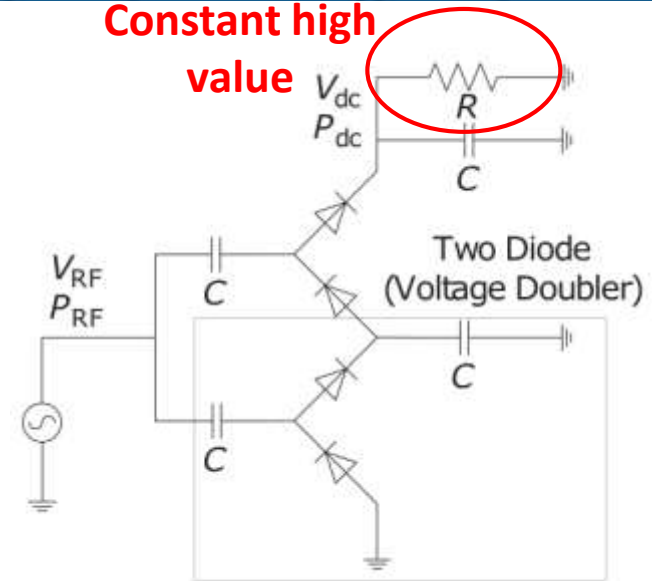


## Batteryless Transponder for Vehicular DSRC at 5.8 GHz

Conventional approach neglect the importance of the nonlinear effects in the rf-to-dc rectifier, with low dynamic termination



Constant high value



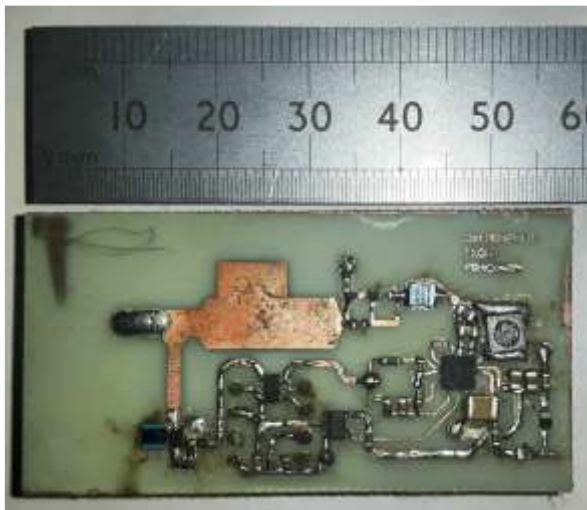
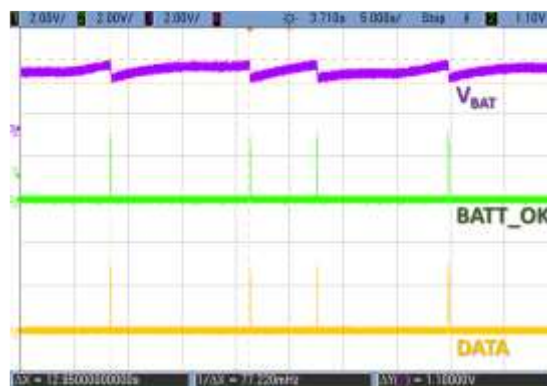


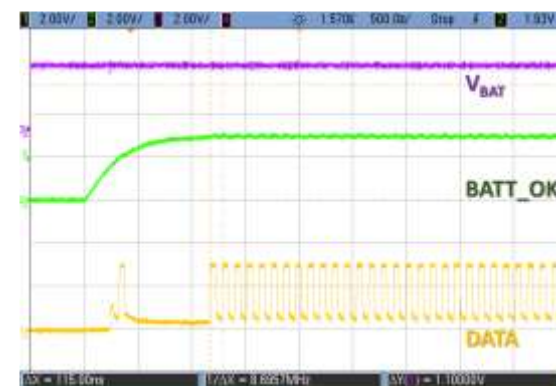
TABLE II: Harvesting performances at comparison with the state-of-the-art

Design	Harvesting Load and Conditions	Measured $P_{DC}$ ( $\mu\text{W}$ )	$\eta$	$I_{CHG}$ ; $\Delta T_{CHG}$
[43]	DC/DC, Current Sink 868 MHz, -5 dBm	-	-	-; 2.5 s
[4]	100 $\Omega$ , fixed load 2.4 GHz, -5 dBm	40.1	13%	118 $\mu\text{A}$ ; -
[2]	3000 $\Omega$ , fixed load 5.8 GHz, -5 dBm	72.7	23%	145 $\mu\text{A}$ ; -
[2]	DC/DC, Current Sink 5.8 GHz, 1 dBm	-	-	-; 140 s
This work	DC/DC, Current Sink 5.8 GHz, -5 dBm	51.0	16%	135 $\mu\text{A}$ ; 37 s
This work	DC/DC, Current Sink 5.8 GHz, -8 dBm	17.0	11%	50 $\mu\text{A}$ ; 100 s

Oscilloscope traces acquired with  $P_{RF} = -5$  dBm  
Cyclic Packet Transmission



Transient of transmitted packet





## Car Talk



Alessandro Cidronali, Stefano Maddio,  
Marco Passafiume, and Gianfranco Manes

**T**he vision for intelligent transportation systems (ITS) in the near term foresees establishing radio communications between vehicles and the road infrastructure using the 5.0-GHz frequency band to propagate useful information aimed at passenger safety and efficient traffic management [1]–[5]. To date, three classes of applications have been distinguished at the communication application layer: road safety, traffic efficiency, and a catch-all category of other applications. All rely on roadside equipment (RSE) capable of broadcasting

other regulatory or contextual information along with onboard units (OBU) capable of exchanging with the RSE and, in some cases, of the information to other vehicles.

In Europe, all these cases, along with are classified by the European Telecommunications Standards Institute (ETSI) [2]. Worldwide years, other applications have been developed to address specific needs of transport and safety. The most relevant are tolls [4], [5] (see “Road Tolls: An Ancient



collection (ETC) for vehicular applications and capable of reconfiguring its parameters according to emerging ITS applications. We present an RSE prototype that uses a mixed-RF digital front end intended for dual-mode operation (namely, ETC and ITS modes) in the 5-GHz band. We address the constraint of maintaining interoperability among







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